APPENDIX 3







WATER CYCLE MANAGEMENT CEDAR GROVE ESTATE STAGE 2



June 2013 Report No. X12064-01 Prepared for White Constructions Pty Ltd









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Brown Consulting (NSW) Pty Ltd

June 2013

DOCUMENT CONTROL

X12064 120518 Water Cycle Report.dotx

Issue	Date	Issue Details	Author	Checked	Approved
A	May 12	Draft Report	TE		
В	Jul 12	Report	TE	RP	
С	Jun 13	Updated Report	TE	RP	



WATER CYCLE MANAGEMENT

CEDAR GROVE STAGE 2

FOR CLIENT

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LIST OF ABBREVIATIONS

AEP Annual Exceedance Probability

AHD Australian Height Datum ARI Average Recurrence Interval ARR Australian Rainfall and Runoff

DIPNR Department of Infrastructure, Planning and Natural Resources

DLWC Department of Land and Water Conservation NSW

DEM Digital Elevation Model DTM Digital Terrain Model

FPDM Floodplain Development Manual

FPLFlood Planning Level

FPMM Floodplain Management Manual **FPRMS** Floodplain Risk Management Study

FSL Flood Surface Level

GIS Geographic Information System

Hectare (Area = 10,000m²) ha LEP Local Environmental Plan LGA Local Government Area

MGA Map Grid Australia

 m^3/s Cubic meters per second **PMF** Probable Maximum Flood

PMP Probable Maximum Precipitation

RCP Reinforced Concrete Pipe

RCBC Reinforced Concrete Box Culvert Roads and Traffic Authority of NSW RTA **SEPP** State Environmental Planning Policy

SMP

Stormwater Management Plan TIN Triangular Irregular Network

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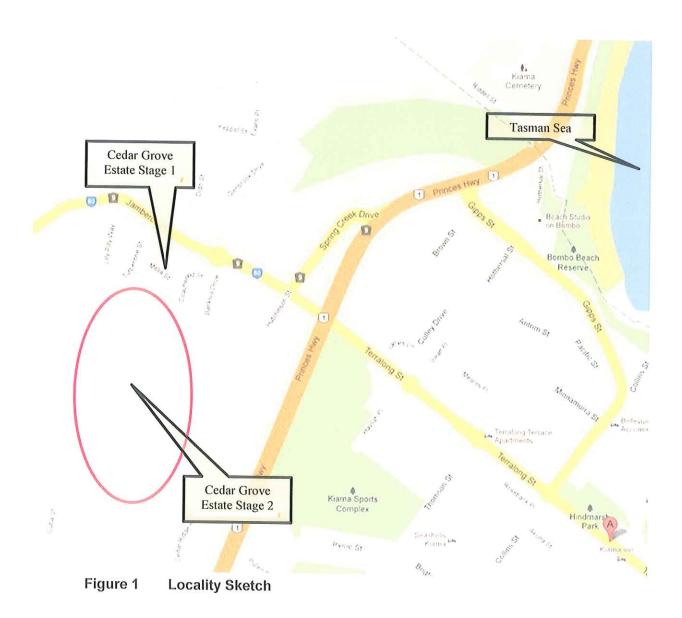


Water Cycle Management

1 INTRODUCTION

Brown Consulting has been engaged by White Constructions Pty Ltd to prepare the Water Cycle Management for Cedar Grove Estate stage 2 to support the rezoning application.

The site is located in Kiama, NSW. Cedar Grove Stage 2 is located south of the Stage I development and bounded to the east by Willow Gully Creek and rural properties to the west. The site drains to Willow Gully Creek with a portion of the western catchments discharge into Spring Creek. The Northern catchments drain to the Cedar Grove Stage I basins (basin I & 2), refer to figure 2.





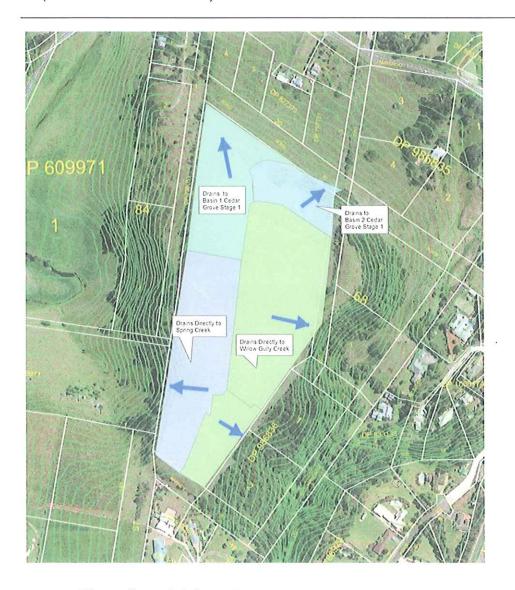


Figure 2 Catchments

1.1 OBJECTIVES

The water cycle management report aims to provide a stormwater strategy suitable for the rezoning of stage 2 Cedar Grove Estates. The report provides a stormwater strategy that is suitable for managing stormwater quantity and quality for a proposed development. Greater detail will be provided during the various design phases.



2 HYDROLOGY

The stormwater masterplan undertaken for Cedar Grove Estate stage I (Brown, 2004) reported on the hydrological modelling of Willow Gully Creek. The study established that the catchments that drain directly to Willow Gully Creek did not require OSD due to the lag time associated with the upstream Catchment. The study showed that development conditions with no OSD did not impact the peak flows in Willow Gully Creek because of the close location to the creek outlet, the Ocean.

Basin I within Stage I Cedar Grove, provided OSD detention for the developed catchment to ensure no aggravating of flows within Spring Creek. The design of basin I and 2 included receiving flows from a portion of the existing stage 2 catchments.

3 DETENTION

The Kiama Municipal Council Water Sensitive Urban Design Policy identifies the On-site retention/ On-site detention requirements for a development. Where rainwater tanks are over 5000 litres and utilised for toilets, laundry and external uses, Council will allow 40% of the rainwater tank volume to be credited to OSD.

3.1 Catchments Draining to Willow Gully Creek

The catchments draining directly to Willow Gully Creek are close to the ocean outlet and will not provide OSD to avoid aligning peak flood levels with the upstream Creek catchments. The lots will provide rainwater tanks for reuse (2000-3000 L) and manage environmental flows, for larger events the flows will discharge directly into Willow Gully Creek.

An XP-RAFTS model was developed to assess the impact of allowing the Willow Gully Creek to discharge uncontrolled. The model parameters were adjusted to match the original Watershed Bounded Network Model (WBNM) prepared for Willow Gully Creek. The modelling showed that the catchment with no OSD would discharge to the ocean prior to the peak flow from the 47ha Willow Gully Creek Catchment arrives. The results presented below show the flow from Subcatchment 4 (including the site catchment) and the outlet for the 100 year ARI storm event.

	Sub catchment 4	Outlet	
	m3/s	m3/s	
Pre-developed	1.96	21.36	
Developed	2.86	20.94	

The results showed although the flow for the site catchment was increased as a result of the development, the peak flow arriving at Jamberoo Road were reduced as a result of a shorter time of concentration.



3.2 Catchments Draining to Cedar Grove Stage 1 Basin 1

Cedar Grove Estate Stage I provided detention storage for all storms up to the 100 year ARI storm event, and included the existing catchment upstream of the developed (stage 2). The proposal for stage 2 Cedar Grove reduces the catchment area draining to the constructed stage I basin I, and therefore a proportion of the storage within the stage I basin can be utilised to manage the flows off stage 2.

The preliminary modelling has shown an OSD component of 410m³ will maintain the flows provided in the stage I design and not aggravate existing flows discharging from the stage I outlet. The OSD volume within stage 2 can be achieved through a number of options including the combination of either/or an OSD storage along the boundary or the lots to provide rainwater tanks with a detention component.

3.3 Catchments Draining to Cedar Grove Stage 1 Basin 2

Cedar Grove Estate Stage I study established that the catchment area draining to basin 2 did not require stormwater detention to ensure peak flood levels downstream were not aggravated as a result of the development. A portion of the stage 2 development is included in the basin 2 catchment area, and will not require On-site detention.

The preliminary modelling has shown an OSD component of 150m³ will maintain the flows provided in the stage I design and not aggravate existing flows discharging from the stage I outlet. The OSD volume within stage 2 can be achieved through a number of options including the combination of either/or an OSD storage along the boundary or the lots to provide rainwater tanks with a detention component.

3.4 Catchments Draining Directly to Spring Creek

The catchments along the western boundary drain directly to Spring Creek and will provide stormwater detention. The Kiama Municipal Council Water Sensitive Urban Design Policy identifies a site storage requirement of 132 m³/ha and permissible site discharge of 600 L/s/ha. Where rainwater tanks are over 5000 litres and utilised for toilets, laundry and external uses, 40% of the rainwater tank volume to be credited to OSD, and the remainder of storage shortfall could be contained within the air gap of the rainwater tank or elsewhere within the lot. Alternatively the OSD component can be contained within a basin downstream of the development prior to discharging into Spring Creek. The proposed lot configuration and detention strategy is subject to detailed design.



4 WATER QUALITY

The Kiama Municipal Council Water Sensitive Urban Design Policy identifies the pollutant removal targets, the targets are as follows;

Pollutant	Target (% Removal)	
Total Suspended Solids (TSS)	80	
Total Nitrogen (TN)	45	
Total Phosphorus (TP)	45	

The Cedar Grove Stage I developed a treatment train to utilise gross pollutant traps and biofiltration basins for treatment of minor storm events (approximately 3 month ARI). The Stage I bio-filtration basin filter surface areas are as follows:

Basin I
 250 m²

Basin 2 385 m²

The results water quality treatment devices showed a significant reduction in developed loads, 91% reduction in suspended solids, 53% reduction in total nitrogen and 63% reduction in total phosphorous.

Preliminary water quality modelling of a proposed development located at Stage 2 Cedar Grove has been undertaken using the Model for Urban Stormwater Improvement Conceptualisation (MUSIC) software package developed by the Cooperative Research Centre for Catchment Hydrology (CRCCH). MUSIC enables the user to model the transfer of pollutants through a catchment and provides an aid in determining the treatment strategy required to meet the water quality objectives applicable to the site. The critical pollutants to be modelled are Gross Pollutants, Total Nitrogen (TN), Total Phosphorous (TP) and Total Suspended Solids (TSS).

The generation, transfer and removal of these critical pollutants will be modelled through a proposed treatment strategy. Only the critical pollutants will be further addressed in this report, however the treatment devices will provide mitigation of other pollutant loads, such as heavy metals, since they are predominantly associated with fine sediment. The Primary Pollutant trap will intercept pollutants such as litter, rubbish, leaves etc therefore minimising the runoff of oxygen demanding substances.

4.1 Catchments Draining to Willow Gully Creek

The catchments draining directly to Willow Gully Creek will utilise rainwater tanks within each lot and bioretention swales. Preliminary modelling suggests a bioretention area of 120 m² (northern outlet) and



40 m² (southern outlet) would be required throughout the catchment, the bioretention can be provided within each lot, within open space or swales within the road corridors.

4.2 Catchments Draining to Cedar Grove Stage 1 Basin 1

The catchment areas draining to basin I stage I utilises the bioretention within the basin. Furthermore the stage 2 lots within the catchment will provide rainwater tanks, and a vegetated buffer strip is located along the boundary upstream of stage I for further treatment.

4.3 Catchments Draining to Cedar Grove Stage 1 Basin 2

The catchment areas draining to basin 2 stage I utilises the bioretention within the basin. Furthermore the stage 2 lots within the catchment will provide rainwater tanks, and a vegetated buffer strip is located along the boundary upstream of stage I for further treatment.

4.4 Catchments Draining Directly to Spring Creek

The catchments draining directly to Spring Creek will utilise rainwater tanks within each lot and bioretention swales. Preliminary modelling suggests a bioretention area of 80 m² would be required throughout the catchment to meet the removal targets, the bioretention can be provided within each lot, open space areas or swales within the road corridors. Alternatively the bioretention can be contained within a basin located downstream of the lots prior to discharging into Spring Creek.

4.5 Removal Efficiencies

Preliminary MUSIC modelling for the rezoning of stage 2 Cedar Grove Estates shows the water quality treatment strategy proposed above will achieve the following pollutant removal;

Pollutant	Inflow (kg/yr)	Outflow (kg/yr)	% Removal	Achieved Target
Total Suspended Solids (TSS)	16400	3130	80.9	Yes
Total Nitrogen (TN)	35.4	10.8	69.5	Yes
Total Phosphorus (TP)	269	144	46.5	Yes
Gross Pollutants (GP)	2260	0	100	Yes



5 CONCLUSION

The stormwater management for the rezoning of Cedar Grove Stage 2 has been prepared in accordance with the Kiama Municipal Council Water Sensitive Urban Design Policy (2005). The stormwater components of the development of the land would be designed to meet the principal including;

- Ensuring peak flows are maintained at a rate not exceeding existing conditions,
- Improve water quality of stormwater discharging from the site such that pollutant loads are no
 worse than existing conditions and meet the removal targets specified by Council,
- Manage environmental flows of Spring Creek and Willow Gully Creek, and
- Promote Water Sensitive Urban Design.

The stormwater management is a conceptual plan for the rezoning, the proposal will be reviewed and detailed for the development application when further details of the subdivision are available.



6 REFERENCES

Brown Consulting (2004). Stormwater Masterplan for Development Application at Cedar Grove Estate, Kiama.

Kiama Municipal Council (2005)Kiama Municipal Council Water Sensitive Urban Design Policy



7 GLOSSARY OF TERMS

Afflux The rise in water level upstream of a hydraulic structure such as a bridge

or culvert, caused by losses incurred from the hydraulic structure.

Australian Height Datum National survey datum corresponding approximately to mean sea level.

Annual Exceedance Probability The chance of a flood of a given size or larger occurring in any one year,

generally expressed as percentage probability. For example, a 100 year ARI flood is a 1% AEP flood. An important implication is that when a 1% AEP flood occurs, there is still a 1% probability that it could occur the

following year.

flood as big as, or larger than the selected flood event.

Catchment at a particular point is the area of land which drains to that

point.

Design floor level The minimum (lowest) floor level specified for a building.

Design flood A hypothetical flood representing a specific likelihood of occurrence (for

example the 100 year or 1% probability flood). The design flood may

comprise two or more single source dominated floods.

Development Existing or proposed works which may or may not impact upon flooding.

Typical works are filling of land, and the construction of roads, floodways

and buildings.

Discharge The rate of flow of water measured in terms of volume over time. It is

not the velocity of flow which is a measure of how fast the water is moving rather than how much is moving. Discharge and flow are

interchangeable.

Digital Terrain Model A three-dimensional model of the ground surface that can be represented

as a series of grids with each cell representing an elevation (DEM) or a

series of interconnected triangles with elevations (TIN).

Effective warning time The available time that a community has from receiving a flood warning to

when the flood reaches their location.

First Flush The initial surface runoff of a rainstorm. During this phase, water

pollution in areas with high proportions of impervious surfaces is typically

more concentrated compared to the remainder of the storm.

Flood Above average river or creek flows which overtop banks and inundate

floodplains.

Flood awareness An appreciation of the likely threats and consequences of flooding and an

understanding of any flood warning and evacuation procedures. Communities with a high degree of flood awareness respond to flood warnings promptly and efficiently, greatly reducing the potential for damage and loss of life and limb. Communities with a low degree of flood awareness may not fully appreciate the importance of flood warnings and flood preparedness and consequently suffer greater personal and

economic losses.

Flood behaviour The pattern / characteristics / nature of a flood.



Flooding The State Emergency Service uses the following definitions in flood

warnings:

Minor flooding: causes inconvenience such as closing of minor roads and the

submergence of low level bridges

Moderate flooding: low-lying areas inundated requiring removal of stock and/or evacuation of some houses. Main traffic bridges may be covered. Major flooding: extensive rural areas are flooded with properties, villages and

towns isolated and/or appreciable urban areas are flooded.

Flood frequency analysis An analysis of historical flood records to determine estimates of design

flood flows.

Flood fringe Land which may be affected by flooding but is not designated as a

floodway or flood storage.

Flood hazard The potential threat to property or persons due to flooding.

Flood level The height or elevation of flood waters relative to a datum (typically the

Australian Height Datum). Also referred to as "stage".

Flood liable land

Land inundated up to the probable maximum flood – flood prone land.

Floodplain Land adjacent to a river or creek which is inundated by floods up to the

probable maximum flood that is designated as flood prone land.

Flood Planning Levels Are the combinations of flood levels and freeboards selected for planning

purposes to account for uncertainty in the estimate of the flood level.

Flood proofing Measures taken to improve or modify the design, construction and

alteration of buildings to minimise or eliminate flood damages and threats

to life and limb.

Floodplain Management The coordinated management of activities which occur on flood liable

land.

Floodplain Management Manual A document by the NSW Government (2001) that provides a guideline for

the management of flood liable land. This document describes the

process of a floodplain risk management study.

Flood source The source of the flood waters.

Floodplain Management A set of conditions and policies which define the benchmark from

Standard which floodplain management options are compared and assessed.

Flood standard The flood selected for planning and floodplain management activities.

The flood may be an historical or design flood. It should be based on an understanding of the flood behaviour and the associated flood hazard. It should also take into account social, economic and ecological

considerations.

Flood storages Floodplain areas which are important for the temporary storage of flood

waters during a flood.

Floodways Those areas of the floodplain where a significant discharge of flow occurs

during floods. They are often aligned with naturally defined channels. Floodways are areas that, even if they are partially blocked, would cause significant redistribution of flood flows, or a significant increase in flood

levels.



Freeboard A factor of safety usually expressed as a height above the flood standard.

Freeboard tends to compensate for the factors such as wave action,

localised hydraulic effects and uncertainties in the design flood levels.

Geographical Information System A form of computer software developed for mapping applications and

data storage. Useful for generating terrain models and processing data for

input into flood estimation models.

High hazard Danger to life and limb; evacuation difficult; potential for structural

damage, high social disruption and economic losses. High hazard areas are those areas subject to a combination of flood depth and flow velocity

that are deemed to cause the above issues to persons or property.

Historical flood A flood which has actually occurred – Flood of Record.

Hydraulic The term given to the study of water flow in rivers, estuaries with coastal

systems.

Hydrograph A graph showing how a river or creek's discharge changes with time.

Hydrology The term given to the study of the rain-runoff process in catchments.

Flood depths and velocities are sufficiently low that people and their

possessions can be evacuated.

Management plan A clear and concise document, normally containing diagrams and maps,

describing a series of actions that will allow an area to be managed in a

coordinated manner to achieve defined objectives.

Map Grid Australia A national coordinate system used for the mapping of features on a

representation of the earths surface. Based on the geographic coordinate

system 'Geodetic Datum of Australia 1994'.

Peak flood level, flow or
The maximum flood level, flow or velocity occurring during a flood

velocity event

Low hazard

Probable Maximum Flood An extreme flood deemed to be the maximum flood likely to occur at a

particular location.

Probable Maximum Precipitation The greatest depth of rainfall for a given duration meteorologically

possible over a particular location. Used to estimate the probable

maximum flood.

Probability A statistical measure of the likely frequency or occurrence of flooding.

Riparian Zone Areas that are located adjacent to watercourses. Their definition is vague

and can be characterised by landform, vegetation, legislation or their

function.

Runoff The amount of rainfall from a catchment which actually ends up as

flowing water in the river of creek.

Stage Equivalent to water level above a specific datum- see flood level.

Stage hydrograph A graph of water level over time.

Triangular Irregular Network A mass of interconnected triangles used to model three-dimensional surfaces

such as the ground (see DTM) and the surface of a flood.

Velocity The speed at which the flood waters are moving. Typically, modelled

velocities in a river or creek are quoted as the depth and width averaged velocity, i.e. the average velocity across the whole river or creek section.



8 APPENDICES

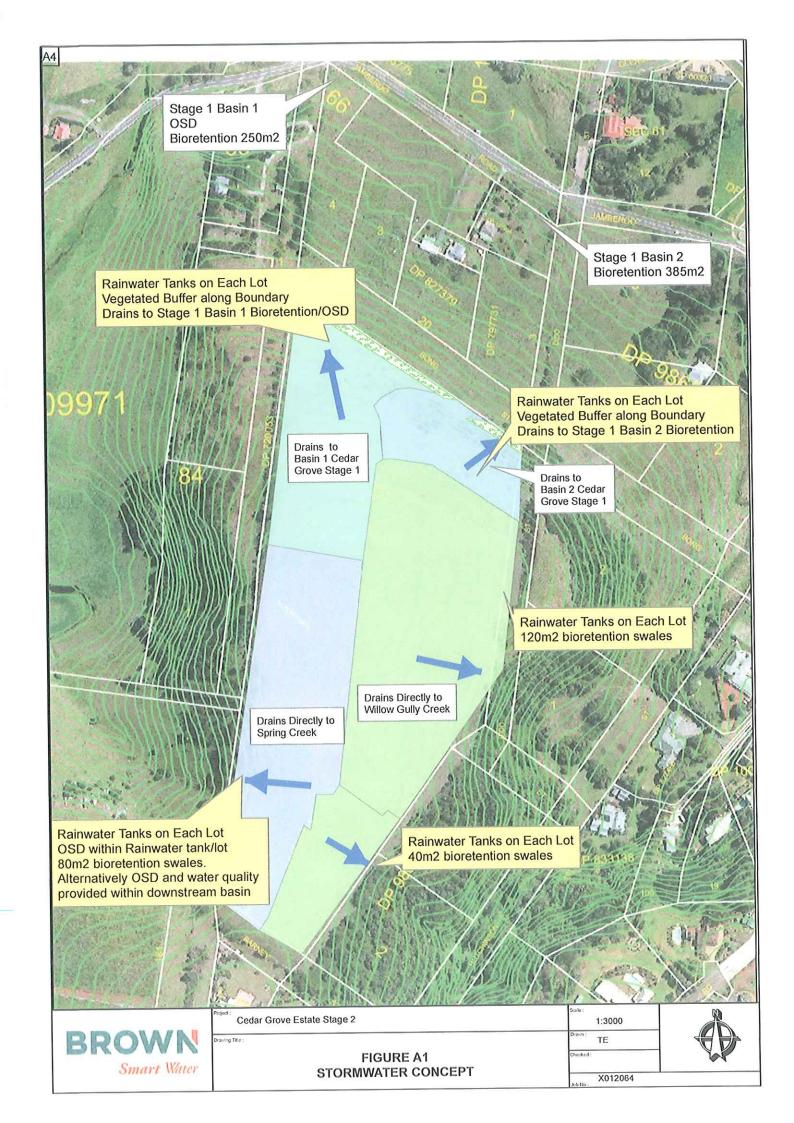
Appendix A

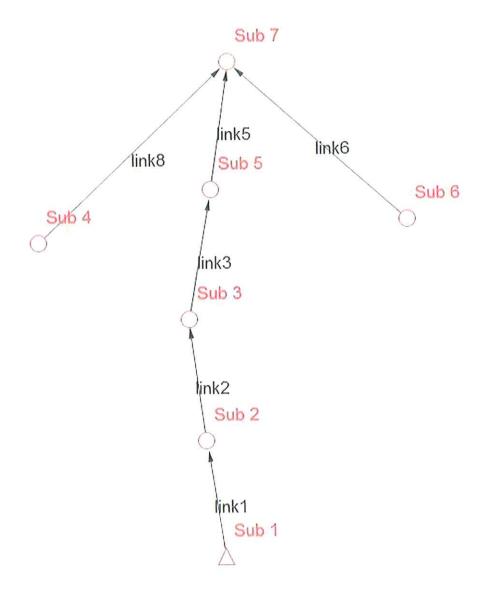
Drawings



APPENDIX A

DRAWINGS





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Max. no. of routng increments allowed = 250000	
Max. no. of rating curve points = 250000	
Max. no. of storm temporal points = 250000	
Max. no. of channel subreaches = 25	
Max link stack level = 50	
Input Version number = 820	
LINK Sub 1 1.000	0 206
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iosd 11kta 0 1 LINK Sub 2 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) = ESTIMATED TIME TO PEAK (MINS) =	25.95 12. 33.00
LINK Sub 3 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) = ESTIMATED TIME TO PEAK (MINS) =	50.92 17. 40.00
LINK Sub 5 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) = ESTIMATED TIME TO PEAK (MINS) =	61.88 19. 47.00
LINK Sub 6 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) = ESTIMATED TIME TO PEAK (MINS) =	2.933 0.92 42.00
LINK Sub 4 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) = ESTIMATED TIME TO PEAK (MINS) = Page 1	4.242 2.0 31.00

willowcreek.out

LINK Sub 7

1.000

ESTIMATED	VOLUME (CU I	METRES*10**3) =	69.05
	PEAK FLOW	(CUMECS) =	21.
ESTIMATED	TIME TO PEAL	$K \qquad (MINS) =$	52.00

Kiama

#####

ROUTING INCREMENT (MINS)	=	1.00	
STORM DURATION (MINS)	=	60.	
RETURN PERIOD (YRS)	=	100.	
BX	=	1.0000	
TOTAL OF FIRST SUB-AREAS	(ha)	=	25.78
TOTAL OF SECOND SUB-AREA	s (ha)	=	40.25
TOTAL OF ALL SUB-AREAS (ha)	=	66.03

SUMM. Link Label	ARY OF CATCHMEN Catch. Area #1 #2		L DATA % Impervious #1 #2 (%)	Pern #1 #2	B #1 #2	Link No.
Sub 1	(ha) 7.524 0.000	1.000 0.000	99.00 0.000	.025 0.00	.0086 0.000	1.000
Sub 2	6.720 10.080	1.000 1.000	99.00 1.000	.025 .045	.0081 .1266	1.001
Sub 3	7.236 16.884	1.000 1.000	99.00 1.000	.025 .045	.0084 .1656	1.002
Sub 5	4.192 6.288	2.000 2.000	99.00 1.000	.025 .045	.0045 .0701	1.003
Sub 6	0.0100 2.900	1.000 1.000	99.00 1.000	.025 .045	.0003 .0662	2.000
Sub 4	0.1000 4.100	3.500 3.500	99.00 1.000	.025 .045	.0005 .0425	3.000
Sub 7	.00001 0.000	1.000 0.000	1.000 0.000	.025 0.00	0.000 0.000	1.004

Link Label		#1 #2 (mm/h)	(mm)	Peak Inflow (m^3/s)	Time Link to Lag Peak mins
Sub 1	113.00 1.500 0.000	0.000 0.000	111.50 0.000	6.167	25.00 7.500
Sub 2	113.00 1.500 10.00	0.000 3.000	111.50 100.40	11.851	33.00 7.000
Sub 3	113.00 1.500 10.00	0.000 3.000	111.50 100.40	16.677	40.00 7.000
Sub 5	113.00 1.500 10.00	0.000 3.000	111.50 100.40	19.339	47.00 5.000
Sub 6	113.00 1.500 10.00	0.000 3.000	111.50 100.40	0.9246	42.00 2.000
Sub 4	113.00 1.500 10.00	0.000 3.000	111.50 100.40	1.961	31.00 5.000
Sub 7	113.00 1.500 0.000	0.000 0.000	111.50 0.000	21.364	52.00 0.000

willowcreek.out

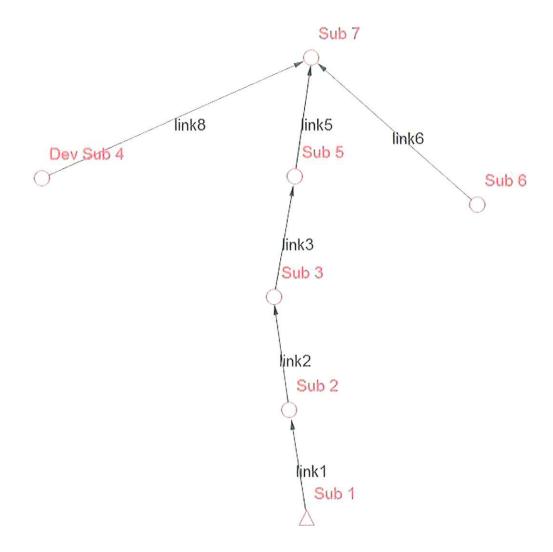
SUMMARY OF BASIN RESULTS

Link	Time	Peak	Time	Peak	Total		Basin -	
Label	to	Inflow	to	outflow	Inflow	Vol.	Vol.	Stage
	Peak	(m^3/s)	Peak	(m^3/s)	$(m \wedge 3)$	Avail	Used	Used
Sub 1		6.167			8385.9	0.0000	996.1	9 69.833

SUMMARY OF BASIN OUTLET RESULTS

Link	No.	S/D	Dia	Width	Pipe	Pipe
Label	of	Factor			Length	slope
		(m)	(m)	(m)	(m)	(%)
Sub 1	1.0	1.000	51 1/31	0.000	20.000	0.2000

Run completed at: 25th June 2013 8:42:55



##### RUNTIME	######################################
Max. no. of links allowed = 10000	
Max. no. of routng increments allowed =	250000
Max. no. of rating curve points = 2	250000
Max. no. of storm temporal points =	250000
Max. no. of channel subreaches =	25
Max link stack level = 50	
Input Version number = 820	
LINK Sub 1 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	8.386 = 6.2 = 25.00
iosd llkta 0 1 LINK Sub 2 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	
LINK Sub 3 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	
LINK Sub 5 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	61.88 = 19. = 47.00
LINK Sub 6 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	2.933 0.92 = 42.00
LINK Dev Sub 4 1.000	
ESTIMATED VOLUME (CU METRES*10**3) = ESTIMATED PEAK FLOW (CUMECS) ESTIMATED TIME TO PEAK (MINS)	

Page 1

willowcreek_dev.out

LINK Sub 7

1.000

ESTIMATED	VOLUME (CU	METRES*10**3) =	69.21
ESTIMATED	PEAK FLOW	(CUMECS) =	21.
ESTIMATED	TIME TO PEA	$K \qquad (MINS) =$	52.00

ROUTING INCREMENT (MINS) =	1.00
STORM DURATION (MINS) =	60.
RETURN PERIOD (YRS) =	100.
BX =	1.0000
TOTAL OF FIRST SUB-AREAS (ha) = 28.27
TOTAL OF SECOND SUB-AREAS (ha) = 37.67
TOTAL OF ALL SUB-AREAS (ha)	= 65.93

SUMMA	ARY OF CA	ATCHMEN ⁻					
Link Label	Catch. #1	Area #2	slope #1 #2	% Impervious #1 #2	Pern #1 #2	B #1 #2	Link No.
	(ha)	11 2	(%)	(%)	112 112	11 11 11 2	110.
Sub 1	7.524	0.000	1.000 0.000	99.00 0.000	.025 0.00	.0086 0.000	1.000
Sub 2	6.720 1	10.080	1.000 1.000	99.00 1.000	.025 .045	.0081 .1266	1.001
Sub 3	7.236 1	16.884	1.000 1.000	99.00 1.000	.025 .045	.0084 .1656	1.002
Sub 5	4.192	6.288	2.000 2.000	99.00 1.000	.025 .045	.0045 .0701	1.003
Sub 6	0.0100	2.900	1.000 1.000	99.00 1.000	.025 .045	.0003 .0662	2.000
Dev Sub 4	2.583	1.517	3.500 3.500	99.00 1.000	.025 .045	.0026 .0253	3.000
Sub 7	.00001	0.000	1.000 0.000	1.000 0.000	.025 0.00	0.000 0.000	1.004

Lab	el	Ir	ntensity (mm/h)	/ #1 (n	#2 nm)	#1 (mm/	#2 /h)	#1 (mm	#2 ı)	Peak Inflow (m^3/s) 6.167	Peak	Lag mins
Sub												
Sub	3		113.00	1.500	10.00	0.000	3.000	111.50	100.40	16.677	40.00	7.000
Sub	5		113.00	1.500	10.00	0.000	3.000	111.50	100.40	19.339	47.00	5.000
Sub	6		113.00	1.500	10.00	0.000	3.000	111.50	100.40	0.9246	42.00	2.000
Dev	Sub	4	113.00	1.500	10.00	0.000	3.000	111.50	100.40	2.865	25.00	5.000
Sub	7		113.00	1.500	0.000	0.000	0.000	111.50	0.000	20.937	52.00	0.000

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Link_	Time	Peak	Time	Peak	Total		Basin -	
Label	to	Inflow	to		Inflow	Vol.	Vol.	Stage
	Peak	(m^3/s)	Peak	(m^3/s)	(m^3)	Avail	Used	Used
Sub 1	25.00	6.167	25.00	7.593	8385.9	0.0000	996.19	9 69.833

SUMMARY OF BASIN OUTLET RESULTS

Link	No.	S/D	Dia	Width	Pipe	Pipe
Label	of	Factor			Length	Slope
.		(m)	(m)	(m)	(m)	(%)
Sub 1	1.0	1.000		0.000	20.000	0.2000

Run completed at: 25th June 2013 8:39:00